Atomic-scale structure of hard-core fluids under shear flow

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The effect of velocity correlations on the equal-time density autocorrelation function, e.g., the pair distribution function (PDF), of a hard-sphere fluid undergoing shear flow is investigated. The PDF at contact is calculated within the Enskog approximation and is shown to be in good agreement with molecular dynamics simulations for shear rates below the shear-induced ordering transition. These calculations are used to construct a nonequilibrium generalized mean-spherical approximation for the PDF at finite separations, which is also found to agree well with the simulation data.

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I. INTRODUCTION

In equilibrium, simple fluids exhibit spatial correlations which are characterized by the pair distribution function (PDF) describing the probability of finding two atoms with a given relative orientation and separation. Equilibrium liquid state theory is primarily concerned with the calculation of the PDF and a number of successful approaches have been developed, including the Percus-Yevik approximation for hard spheres, the mean-spherical approximation, and the more recent self-consistent integral equations [1]. Knowledge of the PDF is equivalent to knowledge of the density-density static correlation function [1] and once this is known, all other interesting static correlation functions, e.g., density-energy and energy-energy static correlation, functions, are immediately known because the velocity dependence of the twobody distribution function in equilibrium is trivial. It is a characteristic of nonequilibrium fluids that this property no longer holds [2-5], and the presence of velocity correlations is the reason that the determination of static correlations in nonequilibrium fluids, over all densities and length scales, is a difficult problem.

The velocity correlations that occur in nonequilibrium fluids, as well as in fluctuations about the equilibrium state, are generated by collisions that have the effect of altering the two-body probability distribution so that even if the velocities of the atoms prior to a collision are assumed to be independent variables, the velocities after a collision are not independent. The question of whether the velocities of two atoms prior to a collision are really independent variables has been much studied in statistical mechanics over the last 30 years and phenomena such as long-time tails and longranged correlations are proof that this assumption is not strictly adhered to [6,7], although in many cases it remains a good approximation. While the calculation of the precollisional correlations is a very difficult problem, it has recently been noted [2] that, for fluids interacting via a hard-core potential, it is possible to calculate the postcollisional correlations in an arbitrary nonequilibrium state for the special case of the two atoms being in contact using the same assumptions as underlie the Enskog theory of the one-body distribution function. This allows one to calculate all static correlation functions for two atoms in contact up to this level of approximation. It was subsequently shown that this information could be combined with a formalism borrowed from equilibrium liquid-state theory to create a successful model of the pair distribution function of a granular fluid [4] (i.e., a fluid of inelastic hard spheres). The purpose of the present paper is to describe an extension of this model to inhomogeneous systems and to examine its application to the particular case of a fluid of elastic hard spheres undergoing uniform shear flow (USF) and to present detailed comparisons of the theory to the result of molecular dynamics simulations. Uniform shear flow, in which the velocity in one Cartesian direction varies linearly with position along another axis, is a particularly interesting example since the density-density correlation function can be studied experimentally by means of light scattering [8]. Furthermore, the hard-sphere model is generally accepted as a reasonable analogy to certain types of colloidal suspensions, see, for example, Ref. [9] and references therein, for which it is possible to achieve conditions of strong shear (e.g., shear rates comparable to the inverse mean free time of the colloidal particles) in the laboratory, which are otherwise inaccessible in simple fluids.

The second section of this paper reviews the theory behind the calculation of static correlations at contact and evaluates the density-density correlation function at contact for the special case of USF. This makes use of recent work on solution of the Enskog equation for high shear rates [10,11] to extend an earlier calculation [2] resulting in an explicit expression for the PDF at contact in a sheared fluid. The third section deals with models for the PDF at finite separations. It reviews two well known theories that are potentially applicable to atomic length scales: the kinetic model studied by Hess and co-workers [12] and the Langevin model of Ronis [13]. The former involves an undetermined parameter which, if the theory is to apply to atomic length scales, can now be fixed by requiring agreement with the calculations for two atoms in contact. The latter, while not involving any a priori unknown parameters is, nevertheless, phenomenological and a diffusion constant appearing in its formulation has in fact been treated as a free parameter when comparing to experiment [8]. Again, it is noted that the pa-

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rameter can be fixed unambiguously by requiring agreement with the calculated value at contact. It is also shown that these two theories are in fact very closely related not withstanding their different motivations. Finally, in this section the nonequilibrium version of the generalized mean spherical approximation (GMSA) is introduced as a means of modeling the PDF at finite separations based on the atomic-length scale information coming from the calculations of Sec. II and, qualitatively, the large-separation (i.e., small wavevector) information provided by mode-coupling theories, based on either kinetic theory [12,14,15] or fluctuating hydrodynamic [13,16,17,18], of which the Ronis theory is an example. This is not unlike the original motivation of Weisman in introducing the equilibrium GMSA as a means of improving on the Percus-Yevik approximation by incorporating accurate knowledge about the PDF at contact, from the Carnahan-Starling equation of state and the pressure equation, to construct a model of the PDF for an equilibrium hard-core fluid accurate over a wide range of densities [19]. Recent work by Yustes and Santos [20-22], as well as Carraro and Ciccariello [23], has shown first that the Percus-Yevik approximation may be viewed as, in some sense, the simplest approximation that provides certain analytic properties that any distribution function must satisfy and second, that the GMSA of Weisman may be viewed as a framework for systematically extending this model so as to incorporate additional constraints. It is with this motivation that the extension of the GMSA to nonequilibrium systems was proposed [3] as a means of modeling the density-density correlation function, i.e., the PDF, at all length scales.

In Sec. IV, these calculations are compared with the results of molecular dynamics (MD) simulations over a wide range of shear rates and densities. As noted previously [2], there seems to be a strong correlation between the rapid decrease, with increasing shear rate, of the PDF in certain directions and the onset of shear-induced ordering of the fluid. Below this transition, it is shown that the Enskog calculations of the PDF at contact are quite accurate at small shear rates and low densities and becomes increasingly inaccurate as the density and/or the shear rate increases. The theories for the PDF at finite separations are also compared to MD and it is found that all three theories are in qualitative agreement with the GMSA providing the best quantitative agreement with simulation. The paper ends with a discussion of the prospects to extend these results to other systems. A preliminary description of some of these results has appeared previously [3].

II. THEORY OF CORRELATIONS AT CONTACT

A. Hard-sphere statistical mechanics

Consider a system of *N* elastic hard spheres of diameter σ in a cubic volume $V = L^3$ described by a Cartesian coordinate system with axes $\hat{\mathbf{x}}, \hat{\mathbf{y}}$ and $\hat{\mathbf{z}}$. The boundary conditions will be discussed below. The dynamics of the atoms consist of free streaming, subject to the boundary conditions, interrupted by elastic collisions. Two atoms having coordinates $\mathbf{q}_i, \mathbf{p}_i$ and $\mathbf{q}_i, \mathbf{p}_i$ at time t_0 will collide at time t_- , provided that σ

 $=|\mathbf{q}_{ij}(t_{-})|$, where $\mathbf{q}_{ij}(t_{-})=\mathbf{q}_{i}(t_{-})-\mathbf{q}_{j}(t_{-})$ and provided $\mathbf{q}_{ij}(t_{-})\cdot\mathbf{p}_{ij}(t_{-})<0$. Immediately after the elastic collision, the momenta become

$$\mathbf{p}_{i}(t_{+}) = \mathbf{p}_{i}(t_{-}) - \hat{\mathbf{q}}_{ij}(t_{-}) [\hat{\mathbf{q}}_{ij}(t_{-}) \cdot \mathbf{p}_{ij}(t_{-})], \qquad (1)$$
$$\mathbf{p}_{j}(t_{+}) = \mathbf{p}_{j}(t_{-}) + \hat{\mathbf{q}}_{ij}(t_{-}) [\hat{\mathbf{q}}_{ij}(t_{-}) \cdot \mathbf{p}_{ij}(t_{-})],$$

so that the relative momentum is reversed along the line of contact and the total momentum is unaffected.

The statistical description of the system is characterized by the *N*-body distribution, $\rho_N(x_1, x_2, \ldots, x_N; t)$ which gives the probability of finding the system at a given phase point, where atom 1 has phase $x_1 \equiv (\mathbf{q}_1, \mathbf{p}_1)$ etc., at the specified time *t*. Its evolution is specified by the pseudo-Liouville equation

$$\begin{bmatrix} \frac{\partial}{\partial t} + \sum_{i=1}^{N} \mathbf{p}_{i} \cdot \frac{\partial}{\partial \mathbf{q}_{i}} + \sum_{i$$

where the collision operator is given by [24]

$$\overline{T}_{-}(ij) = \delta(q_{ij} - \sigma) [\hat{b}_{ij} - 1] \Theta(-\mathbf{q}_{ij} \cdot \mathbf{p}_{ij}), \qquad (3)$$

where the effect of the momentum transfer operator \hat{b}_{ij} on an arbitrary function is to replace the relative momentum \mathbf{p}_{ij} by its postcollisional value $\mathbf{p}_{ij} - 2\hat{\mathbf{q}}_{ij}(\hat{\mathbf{q}}_{ij} \cdot \mathbf{p}_{ij})$ [see Eq. (1)]. The final term of Eq. (2) describes any external one-body forces acting on the atoms. Integrating Eq. (2) over N-n of the coordinates yields the *n*th equation of the Bogoliubov-Born-Green-Kirkwood-Yvon (BBGKY) hierarchy, which relates the *n*-body distribution to the (n+1)-body distribution. In particular, the result of choosing n=N-1 is

$$\begin{bmatrix} \frac{\partial}{\partial t} + \mathbf{p}_1 \cdot \frac{\partial}{\partial \mathbf{q}_1} + \frac{\partial}{\partial \mathbf{p}_1} \cdot \mathbf{F}(x_1) \end{bmatrix} \rho_1(x_1;t)$$

= $-(N-1) \int d\mathbf{q}_{12} \delta(q_{12} - \sigma)$
 $\times [\hat{b}_{12} - 1] \Theta(-\mathbf{q}_{12} \cdot \mathbf{p}_{12}) \rho_2(x_1, x_2;t).$ (4)

If the two-body distribution on the right is approximated by $\rho_2(x_1, x_2; t) \approx \rho_1(x_1; t) \rho_1(x_2; t) g(\mathbf{q}_1, \mathbf{q}_2; t)$, the result is the well-known Enskog equation for the one-body distribution of a system of hard spheres [here, $g(\mathbf{q}_1, \mathbf{q}_2; t)$ is the probability to find two atoms at positions \mathbf{q}_1 and \mathbf{q}_2 and is normally approximated by the equivalent local equilibrium function]. In fact, examination of Eq. (4) shows that the necessary approximation is actually

$$\delta(q_{12} - \sigma)\Theta(-\mathbf{q}_{12} \cdot \mathbf{p}_{12})\rho_2(x_1, x_2; t)$$

$$\approx \delta(q_{12} - \sigma)\Theta(-\mathbf{q}_{12} \cdot \mathbf{p}_{12})\rho_1(x_1; t)\rho_1(x_2; t)$$

$$\times g_0(\mathbf{q}_1, \mathbf{q}_2; t), \qquad (5)$$

which is a somewhat weaker approximation than the assumption that the two-body distribution always factorizes: rather, one need only assume that it factorizes for the case that the two atoms are in contact and approaching one another, which is to say, just prior to a collision. This is a precise statement, for hard spheres, of Boltzmann's "assumption of molecular chaos." Immediately after a collision, the direction of the relative momentum is reversed and the momenta of the two atoms are obviously correlated. In fact, it has been shown [4] that the approximation given in Eq. (5) implies the form of the entire two-body distribution at contact, given by

$$\delta(q_{12} - \sigma)\rho_2(x_1, x_2; t)$$

$$\simeq \delta(q_{12} - \sigma)\rho_1(x_1; t)\rho_1(x_2; t)g_0(\mathbf{q}_1, \mathbf{q}_2; t)$$

$$+ \delta(q_{12} - \sigma)\Theta(\mathbf{q}_{12} \cdot \mathbf{p}_{12})[\hat{b}_{12} - 1]$$

$$\times \rho_1(x_1; t)\rho_1(x_2; t)g_0(\mathbf{q}_1, \mathbf{q}_2; t).$$
(6)

The distribution is seen to have two parts: the first term on the right describing uncorrelated atoms, and the second term describing velocity correlations which arise because of collisions. In equilibrium, the second term vanishes but for nonequilibrium systems, it is generally present and can give rise to substantial structural effects as will be discussed below. This relation is critical in that it can be used to calculate, to the same level of approximation as is inherent in the Enskog equation, any static two-body correlation function at contact.

Finally, the nonequilibrium pair distribution function is defined, as in equilibrium, by

$$g(\mathbf{q}_1, \mathbf{q}_2; t) = V \int d\mathbf{p}_1 d\mathbf{p}_2 \rho_2(x_1, x_2; t).$$
(7)

From the definition of the local density field,

$$n(\mathbf{r}) = \sum_{i=1}^{N} \delta(\mathbf{r} - \mathbf{q}_i), \qquad (8)$$

it follows that the PDF is related to the density autocorrelation function via the usual relationship,

$$\langle n(\mathbf{r})n(\mathbf{r}');t\rangle = n\,\delta(\mathbf{r}-\mathbf{r}') + n^2g(\mathbf{r},\mathbf{r}';t),$$
 (9)

where the brackets indicate an average over the (timedependent) two-body distribution function.

B. Uniform shear flow

To induce shear flow, modified periodic boundary conditions are used [25]. In the x and z directions, periodic boundaries are applied whereas in the y direction, an atom with coordinates $\mathbf{q}_i = (x_i, y_i, z_i)$ and momentum \mathbf{p}_i $= (p_{xi}, p_{yi}, p_{zi})$ will have images with $\mathbf{q} = (x_i + aLt, y_i + L, z_i)$ and $\mathbf{p} = (p_{xi} + aL, p_{yi}, p_{zi})$, where t is the time and the parameter a, having the units of inverse time, is the shear rate. These are just periodic boundaries applied to the coordinates $\mathbf{q}'_i = \mathbf{q}_i - aty_i \hat{\mathbf{x}}$ and $\mathbf{p}'_i = \mathbf{p}_i - ay_i \hat{\mathbf{x}}$, which are the atomic coordinates in the local rest frame of a system undergoing uniform shear flow and are the standard means by which such a flow is simulated.

It is known [10] that this combination of dynamics and boundary conditions allows for an exact solution of the macroscopic conservation laws in which the local density is constant, the local flow velocity is given by $\mathbf{v}(\mathbf{r}) = ar_y \hat{\mathbf{x}}$ and the local temperature, defined as the excess kinetic energy relative to the flow field, is spatially uniform in the comoving frame and increases as

$$\frac{3}{2}nk_B\frac{\partial}{\partial t}T = -aP_{xy} + F, \qquad (10)$$

where P_{ij} is the macroscopic pressure tensor, which is also spatially uniform, and the last term on the right represents the effect of the external forces. Typically, an external force, or thermostat, is included such that the right hand side of this equation vanishes, thus giving a constant temperature and allowing for the possibility of a stationary state. Here, it is assumed that for shear rates below the ordering transition, all thermostats are equivalent [26,27].

The one-body distribution function of a sheared and thermostated fluid of hard spheres has been studied in considerable detail [10,11], and may be approximated as

$$f(\mathbf{q},\mathbf{p}) = \rho \left(\frac{\beta}{2\pi}\right)^{3/2} \left[\det(\Delta)\right]^{-1/2} \exp\left(-\frac{1}{2}\beta p_i' p_j' \Delta_{ij}^{-1}\right),$$
(11)

$$\Delta_{ij} = \delta_{ij} + A_{ij}, \qquad (12)$$

where the (constant) matrix of coefficients is defined implicitly as the solution of

$$a(\delta_{xi}\delta_{jy} + \delta_{yi}\delta_{jx} + \delta_{xi}A_{jy} + \delta_{xj}A_{iy}) = C_{ij}^{(0)} + C_{ij,lm}^{(1)}A_{lm},$$
(13)

with

$$C_{ij}^{(0)} = \rho \chi \int d\mathbf{q} \delta(q-1) q_i q_j \\ \times \left\{ \frac{1}{\sqrt{\pi}} w^2 e^{-w^2/4} + \frac{1}{2} (w^2+2) \psi(w) \right\}, \\ C_{ij,lm}^{(1)} = \frac{1}{2} \rho \chi \int d\mathbf{q} \delta(q-1) \left[\left\{ \frac{8}{\sqrt{\pi}} e^{-w^2/4} + 6 \psi(w) \right\} q_i q_j q_l q_m + \left\{ \frac{2}{\sqrt{\pi}} e^{-w^2/4} + \psi(w) \right\} \Delta_{ijlm} \right], \\ + \left\{ \frac{2}{\sqrt{\pi}} e^{-w^2/4} + \psi(w) \right\} \Delta_{ijlm} \right],$$
(14)
$$\Delta_{ijlm} = (\delta_{il} q_j q_m + \delta_{im} q_j q_l + \delta_{jl} q_i q_m + \delta_{jm} q_i q_l),$$

$$\psi(w) = w \left[\operatorname{erf} \left(\frac{w}{2} \right) - 1 \right],$$
$$w = a q_x q_y,$$

together with the condition that Tr(A) = 0. This approximation gives a semiquantitative description of effects of strong shear such as shear thinning and normal stresses as well as being positive definite at all shear rates. The PDF at contact within this approximation is found to be

$$\delta(r_{12} - \sigma)g(\mathbf{r}_{1}, \mathbf{r}_{2}) = \delta(r_{12} - \sigma)\chi_{0} \left[1 - \operatorname{erf} \left(\frac{1}{2\sigma^{2}} \frac{ar_{12x}r_{12y}}{\sqrt{1 + A_{lm}r_{12l}r_{12m}}} \right) \right], \quad (15)$$

which follows directly from Eqs. (13) and (6). Here and below, χ_0 is taken to be the equilibrium value of the PDF at contact as calculated in the Carnahan-Starling approximation. From this, the projections of the PDF at contact onto the spherical harmonics may be calculated as

$$M_{lm} \equiv \int d\mathbf{r}_{12} Y_{lm}^*(\hat{\mathbf{r}}_{12}) \,\delta(r_{12} - \sigma) g(\mathbf{r}_1, \mathbf{r}_2). \tag{16}$$

Note that from this point, the dependence of all quantities on time is being suppressed since we work in a steady state.

III. THE NONEQUILIBRIUM PAIR DISTRIBUTION FUNCTION

The Enskog approximation gives information about quantities at contact. In order to understand the PDF for finite separations, several different approaches have been suggested. Two well-known proposals, the kinetic model of Hess [12] and the fluctuation model of Ronis [13], involve phenomenological parameters which can be fixed by requiring that they reproduce one of the moments M_{lm} as calculated from Eq. (16). These theories share the property that in equilibrium, they reduce to the equilibrium PDF so that it is reasonable to attempt to reproduce local information such as the moments at contact. This contrasts with calculations of the density autocorrelation function based on kinetic theory [14,15] or, equivalently, long-wavelength Langevin models [18] which can only give information at asymptotically large separations for which the information at contact is not relevant.

A. Kinetic model

The second equation of the BBGKY hierarchy is

$$\frac{\partial}{\partial t}\rho_{2}(x_{1},x_{2};t) + \sum_{i=1,2} \left(\mathbf{p}_{i}^{\prime} \cdot \frac{\partial}{\partial \mathbf{q}_{i}} + \mathbf{q}_{i} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_{i}} + \frac{\partial}{\partial \mathbf{p}_{i}^{\prime}} \cdot \mathbf{F}(x_{i}) \right)$$
$$\times \rho_{2}(x_{1},x_{2};t) + \overline{T}_{-}(12)\rho_{2}(x_{1},x_{2};t)$$
$$= -N \int d3[\overline{T}_{-}(13) + \overline{T}_{-}(23)]\rho_{3}(x_{1},x_{2},x_{3};t), \quad (17)$$

and integrating over the momenta gives an equation for the pdf

$$\frac{\partial}{\partial t}g(\mathbf{q}_{12};t) + \mathbf{q}_{12} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_{12}}g(\mathbf{q}_{12};t)$$
(18)

$$= -\int d\mathbf{p}_{1}d\mathbf{p}_{2}\bar{T}_{-}(12)\rho_{2}(x_{1},x_{2};t) - n\int d\mathbf{p}_{1}d\mathbf{p}_{2}$$
$$\times \int d3[\bar{T}_{-}(13) + \bar{T}_{-}(23)]\rho_{3}(x_{1},x_{2};t).$$
(19)

The kinetic models studied by Hess [12] consist in replacing the complicated right-hand side of this equation by a simpler diffusion or relaxation model constrained only by the requirement that it force a relaxation towards the equilibrium state. This is intended to simplify the complex three-body term while capturing the fundamental physical property that, in the absence of shear, it is the collisions, represented by this term, which tend to drive the PDF to the equilibrium state. The simplest model then takes the form,

$$\frac{\partial}{\partial t}g(\mathbf{q}_{12};t) + \mathbf{q}_{12} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_{12}}g(\mathbf{q}_{12};t)$$
$$= -\Gamma[g(\mathbf{q}_{12};t) - g_0(q_{12})], \qquad (20)$$

where Γ is a relaxation time. Fourier transforming gives

$$\frac{\partial}{\partial t} \widetilde{g}(\mathbf{k}_{12};t) - \mathbf{k}_{12} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{k}_{12}} \widetilde{g}(\mathbf{k}_{12};t)$$
$$= -\Gamma[\widetilde{h}(\mathbf{k}_{12};t) - \widetilde{h}_0(k_{12})].$$
(21)

The solution to Eq. (20), under the assumption of stationarity, is

$$g(\mathbf{q}_{12}) = \int_0^\infty d\gamma e^{-\gamma} g_0[q_{12}(a\gamma\Gamma)], \qquad (22)$$

where

$$\mathbf{q}_{12}(a\,\gamma) = (q_{12x} - a\,\gamma q_{12y}, q_{12y}, q_{12z}). \tag{23}$$

In Fourier space, this becomes the solution to Eq. (21),

$$\widetilde{g}(\mathbf{k}_{12}) = \int_0^\infty d\,\gamma e^{-\,\gamma} \widetilde{g}_0[k_{12}(-a\,\gamma\Gamma)],$$

with

$$\mathbf{k}_{12}(-a\,\gamma\Gamma) = (k_{12x}, k_{12y} + a\,\gamma\Gamma k_{12x}, k_{12z}).$$
(24)

As alluded to above, the relaxation time appearing in this model can be fixed by requiring that the model reproduce one of the moments M_{lm} .

B. Langevin model for density fluctuations

The Langevin model of Ronis [13] consists of a convective-diffusion equation for the decay of density fluctuations which, in Fourier space, appears as

$$\frac{\partial}{\partial t} \,\delta n(\mathbf{k},t) - \mathbf{k} \cdot \vec{a}^T \cdot \frac{\partial}{\partial \mathbf{k}} \,\delta n(\mathbf{k},t) + D(k)k^2 \,\delta n(\mathbf{k},t) = f(\mathbf{k},t),$$
(25)

where D(k) is a wave-vector-dependent diffusion constant and $f(\mathbf{k},t)$ is a fluctuating force representing the neglected degrees of freedom. The fluctuating force is approximated as δ function correlated in both wave vector and time, with amplitude $D(k)S_0(k)k^2$ where $S_0(k)$ is the equilibrium static structure factor. The PDF is obtained by solving for the density fluctuation as a functional of the force and evaluation of the equal-time density-density correlation function with the result

$$\widetilde{h}(\mathbf{k}_{12}) = \int_0^\infty d\gamma D(k(-a\gamma))h_0(k(-a\gamma))k^2(-a\gamma)$$
$$\times \exp\left(-\int_0^\gamma d\gamma' D(k(-a\gamma'))k^2(-a\gamma')\right),$$
(26)

so that it is seen that the particular choice for the autocorrelation of the force leads to the correct result in equilibrium. The similarity between this and the Hess' model is apparent and in fact the same result is obtained if the relaxation time in the latter, Eq. (21), is taken to be wave-vector dependent with $\Gamma(k) = D(k)k^2$. To close the model, Ronis uses D(k) $= D_0/S_0(k)$ with D_0 a constant that he takes to be the equilibrium self-diffusion constant, although in the present circumstances it will be fixed by the requirement that the model give the correct value of M_{22} (the dominant nonequilibrium moment). Finally, the nonequilibrium correction can be written more explicitly by means of an integration by parts, which gives

$$\widetilde{h}(\mathbf{k}_{12}) - \widetilde{h}_0(\mathbf{k}_{12})$$

$$= a \int_0^\infty d\gamma \frac{k_x k_y(-a\gamma)}{k(-a\gamma)} h'_0(k(-a\gamma))$$

$$\times \exp\left(-\int_0^\gamma d\gamma' D(k(-a\gamma'))k^2(-a\gamma')\right),$$
(27)

where $h'_0(k) \equiv (d/dk)h_0(k)$. The same result has recently been derived [28] using a random phase approximation in the context of a Langevin model for the atomic coordinates.

C. Nonequilibrium GMSA

As in equilibrium, define the direct correlation function as usual through the Ornstein-Zernike (OZ) equation

$$h(\mathbf{r}_1,\mathbf{r}_2) = c(\mathbf{r}_1,\mathbf{r}_2) + \int d\mathbf{r}_3 c(\mathbf{r}_1,\mathbf{r}_3)\rho(\mathbf{r}_3)h(\mathbf{r}_3,\mathbf{r}_2),$$
(28)

where $h(\mathbf{r}_1, \mathbf{r}_2) = g(\mathbf{r}_1, \mathbf{r}_2) - 1$ is the structure function. The PDF must satisfy the boundary condition that the probability for two atoms to interpenetrate is zero so that

$$h(\mathbf{r}_1, \mathbf{r}_2) = -1, \ |\mathbf{r}_1 - \mathbf{r}_2| < \sigma.$$
⁽²⁹⁾

The OZ equation can be solved for both the structure function and the direct correlation function (DCF), provided that this is supplemented by a closure relation between the two.

In equilibrium, the relation between the PDF and the direct correlation function may be written as

$$c(\mathbf{r}_{1},\mathbf{r}_{2}) = \ln g(\mathbf{r}_{1},\mathbf{r}_{2}) - h(\mathbf{r}_{1},\mathbf{r}_{2}) + v(\mathbf{r}_{1},\mathbf{r}_{2}) + B(\mathbf{r}_{1},\mathbf{r}_{2})$$
(30)

where $v(\mathbf{r}_1,\mathbf{r}_2)$ is the pair potential and $B(\mathbf{r}_1,\mathbf{r}_2)$ is the bridge function which is not generally known in closed form. The integral equation approach to liquid state structure can be written in terms of various approximations to the bridge function. Setting B=0 yields the hyper-netted chain equation and further approximating $\ln g = \ln[1+h] \approx h$, or B = h-ln(g), yields the Percus-Yevik approximation. A number of other approximations exist, including schemes such as that of Rogers and Young [29] and of Zerah and Hansen [30], which involve a parametrization of the right hand side of Eq. (30). For hard-core potentials, the Percus-Yevik approximation reduces to the statement $c(\mathbf{r}_1,\mathbf{r}_2)=0$ for $|\mathbf{r}_1-\mathbf{r}_2| > \sigma$ and the GMSA replaces the right-hand side by a Yukawa function with parameters adjusted to give a known equation of state. In this case, these have been shown to be the first two steps in a systematic expansion of the tail of the DCF with little underlying physical approximation [20-23]. It thus becomes natural to carry over this model to the nonequilibrium state so that the closure condition is expressed in terms of a similar parametrization of the tail of the DCF giving the form

$$c(\mathbf{r}_1,\mathbf{r}_2) = \sum_i A_i K_i(\mathbf{r}_1,\mathbf{r}_2), \ |\mathbf{r}_1 - \mathbf{r}_2| > \sigma, \qquad (31)$$

for some set of basis functions $\{K_i(\mathbf{r}_1, \mathbf{r}_2)\}$. As it stands, Eq. (31) is quite general and the physical approximation will be to truncate and parametrize this expansion as discussed below.

The problem of solving the OZ equation is now formally equivalent to that of the case of molecular fluids and similar techniques can be used [31]. To begin, one expands the angular dependence of the DCF, the PDF, and the boundary conditions in terms of spherical harmonics so that

$$h(\mathbf{r}_{1},\mathbf{r}_{2};t) = \sum_{lm} h_{lm}(r_{12};t)Y_{lm}(\hat{r}_{12}), \qquad (32)$$

with similar expansions for the other quantities. Using Rayleigh's expansion of a plane wave in terms of radial and angular functions and the addition theorem for spherical harmonics, it is easy to show [31] that the Fourier transform of such an expansion has the form

$$\tilde{h}(\mathbf{k}_1, \mathbf{k}_2; t) = (2\pi)^3 \,\delta(\mathbf{k}_1 + \mathbf{k}_2) \sum_{lm} \bar{h}_{lm}(k_1; t) Y_{lm}(\hat{\mathbf{k}}_1),$$
(33)

with the coefficients defined in terms of Hankel transforms

$$\bar{h}_{lm}(k;t) = 4\pi i^l \int_0^\infty r^2 dr \, j_l(kr) h_{lm}(r).$$
(34)

The Fourier transform of the OZ equation then becomes

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$$\bar{h}_{lm}(k) = \bar{c}_{lm}(k) + n\bar{c}_{l'm'}(k)\bar{h}_{l''m''}(k) \int d\mathbf{\hat{k}}Y_{l'm'}(\mathbf{k})Y_{l''m''}(-\mathbf{k})Y_{lm}^{*}(\mathbf{k})$$

$$= \bar{c}_{lm}(k) + n\frac{1}{\sqrt{4\pi}}\sum_{|l'-l''| \le l \le l'+l''}\sum_{m'=-l'}^{l'}A(l,l',l'',m,m')\bar{c}_{l'm'}(k)\bar{h}_{l''m-m'}(k), \qquad (35)$$

where

$$A(l,l',l'',m,m') = (-1)^{l'+2m} \sqrt{\frac{(2l'+1)(2l''+1)}{2l+1}} C(l',l'',l|000) C(l',l'',l|m',m-m',m)$$
(36)

and the last line is a well-known result that follows from the Wigner-Eckart theorem [32]. Equation (35) together with Eq. (31) and the exact condition, Eq. (29), serve to define the integral equation.

In the theory of molecular liquids [31], auxiliary functions are usually defined as

$$f_{lm}'(r) = \begin{cases} \frac{4\pi i}{(2\pi)^3} \int_0^\infty k^2 dk \frac{\sin(kr)}{kr} \overline{f}_{lm}(k), & l \text{ even} \\ \\ \frac{4\pi i}{(2\pi)^3} \int_0^\infty k^2 dk \frac{\cos(kr)}{kr} \overline{f}_{lm}(k), & l \text{ odd,} \end{cases}$$
(37)

where $\overline{f}_{lm}(k)$ could be either $\overline{h}_{lm}(k)$ or $\overline{c}_{lm}(k)$. For even values of l, the only ones of concern below, this means that the Hankel transform of the original functions is the Fourier-transform of the auxiliary function. This is useful for numerical work but more important is that the auxiliary functions tend to be of shorter range than the original functions. To see this, we need the relation between the auxiliary functions and original functions in real space,

$$f'_{lm}(r) = f_{lm}(r) - \int_{r}^{\infty} r'^{2} dr' \frac{1}{rr'^{2}} P'_{l}(r/r') f_{lm}(r'), \quad (38)$$

where $P'_l(u)$ is the derivative of the *l*th Legendre polynomial with respect to its argument. Direct calculation shows that if $f_{lm}(r) = r^{-n}$ then $f'_{lm}(r) = 0$ provided that 2 < n < l + 3. This transformation therefore removes a subset of long-ranged decays and is consequently degenerate. The inverse transformation is

$$f_{lm}(r) = (-1)^{l} f'_{lm}(r) - (-1)^{l} \\ \times \int_{0}^{r} r'^{2} dr' \frac{1}{r^{2}r'} P'_{l}(r'/r) f'_{lm}(r') \\ + \sum_{n=1}^{[(l-1)/2]} A_{lm,n} r^{-(2n+1)},$$
(39)

where the relationship holds for any choice of the coefficients $A_{lm,n}$ —an expression of the degeneracy of the original transformation. In the present application, since $h_{lm}(0)$ is known, from Eq. (29), we will always have $A_{lm,n}=0$ whereas for the DCF, no such statement can be made.

Further discussion of the details of the solution of these equations is given in the Appendix and only some of the conclusions of that analysis are stated here. First, because of the symmetry of the boundary conditions, only coefficients corresponding to even values of l and m will be nonzero. Second, one expects that, because of the symmetry of the flow, the dominant nonequilibrium contributions come from l=2 and $m=\pm 2$ (since $Y_{22}+Y_{2-2}\propto \hat{xy}$) and indeed this can be verified for the PDF at contact by calculations using Eq. (15). In the case that we keep only these contributions to the OZ equation, as well as the l = m = 0 component necessary to describe the equilibrium contribution, the problem can be transformed into the solution of two one-dimensional OZ equations with the Yukawa closure and an analytic solution is possible as described in the Appendix. This approximation should be understood in the spirit of a truncation of a moment solution rather than an expansion in the shear rate and in fact, all of the expressions presented below depend nonlinearly on the shear rate. The result is that

$$h(\mathbf{r}) = h_{00}(r) Y_{00}(r) + 2h_{22,r}(r) \operatorname{Re} Y_{22}(\hat{\mathbf{r}})$$

$$- 2h_{22,i}(r) \operatorname{Im} Y_{22}(\hat{\mathbf{r}})$$

$$= \frac{1}{\sqrt{4\pi}} h_{00}(r) + \sqrt{\frac{5}{8\pi}} \operatorname{Re}(h_{22}(r))(\hat{r}_{x}^{2} - \hat{r}_{y}^{2})$$

$$- \sqrt{\frac{5}{2\pi}} \operatorname{Im}(h_{22}(r)) \hat{r}_{x} \hat{r}_{y}, \qquad (40)$$

where the angular average of the PDF is given by

$$h_{00}(r) = \frac{\sqrt{4\pi}}{2n} [n_{+}h_{+}(r;n_{+}) + n_{-}h_{-}(r;n_{-})], \quad (41)$$

with $n_{\pm} = n[1 \pm |c| \sqrt{1/4\pi \text{Im}(B_{22,1})}]$ and where the constant, $B_{22,1}$, is related to $A_{22,1}$ occuring in Eq. (39). As discussed in detail in the Appendix, the functions $h_{\pm}(r;n)$ may be expressed in terms of the solution of the OZ equation for *homogeneous* system [e.g., the Percus-Yevik solution if the right-hand side of Eq. (31) is set to zero or the known analytic solution of the N-Yukawa closure [33] if the basis functions are Yukawa terms] for density n_{\pm} . The anisotropic component is given by

$$h_{22}(r) = \Theta(r-1) \left[h'_{22}(r';t) + \frac{B_{22,1}}{r^3} - \frac{3}{r^3} \int_1^r r'^2 dr' h'_{22}(r';B_{22,1}) \right], \quad (42)$$

$$\operatorname{Im}(h_{22}'(r;B_{22,1})) = \frac{\sqrt{4\pi}}{2|a|n} [n_{+}h_{+}(r;n_{+}) - n_{-}h_{-}(r;n_{-})],$$
$$\operatorname{Re}(h_{22}'(r)) = \operatorname{Im}(h_{22}'(r))\operatorname{Re}(M_{22})/\operatorname{Im}(M_{22}).$$

Aside from the truncation of the OZ hierarchy, these results are independent of any assumption about the closure condition given in Eq. (31).

In equilibrium, the GMSA is based on the choice of a Yukawa function for the tail of the DCF. This is motivated by the expectation that the tail is short ranged and, then, because a Yukawa closure is analytically tractable. As discussed above, recent work has shown that the Yukawa term may be thought of as the first term in a systematic expansion thus removing some of the arbitrarity of this choice. In the same spirit, we therefore conclude, as the principal hypothesis of the extension of the GMSA to nonequilibrium systems, that the tail of the auxiliary DCF function can be expanded as

$$\Theta(r_{12}-\sigma)c'(\mathbf{r}_1,\mathbf{r}_2) = \sum_{l,m} v'_{lm}(r_{12})Y_{lm}(\hat{\mathbf{r}}_{12}) \qquad (43)$$

with

$$v'_{lm}(r) \simeq \frac{1}{r} K_{lm} \exp(-z_{lm} r).$$
(44)

For the spherically symmetric component l=m=0 this is just the Yukawa closure as in equilibrium. Because of the nonuniqueness of the relation between the DCF and the auxiliary DCF, see the discussion after Eq. (39), this corresponds to a closure of the actual DCF of the form

$$\Theta(r_{12} - \sigma)c_{lm}(\mathbf{r}_1, \mathbf{r}_2) = v_{lm}(r_{12}) + \sum_{n=1}^{[(l-1)/2]} A_{lm,n}r^{-(2n+1)}.$$
(45)

Since the DCF is of no significance in the present context, the values of $A_{lm,n}$ are left indeterminate at this stage.

As formulated, the truncated analytic model has five parameters corresponding to the amplitudes and length scales of the two Yukawa terms and the constant $B_{22,1}$ appearing in

Eqs. (40)–(42). These parameters are constrained by two boundary conditions consisting of the values of M_{00} and M_{22} . In the first application to shear flow [3], the model was simplified by setting $K_{00}=K_{22}=0$. The justification for this was simplicity, since there is then only the nonuniqueness parameter, $B_{22,1}$, and it was shown that a value could be found which simultaneously satisfied both boundary conditions reasonably well. However, recent estimates [34] indicate that $h_{22}(r)$ decays faster than $1/r^3$ for large *r* leading to the condition that the inverse-cube terms in Eq. (42) vanish in the limit $r \rightarrow \infty$ giving the constraint

$$B_{22,1} = 3 \int_{1}^{\infty} r'^{2} dr' h'_{22}(r'; B_{22,1}), \qquad (46)$$

This still leaves two parameters undetermined. One of these will be eliminated by taking the length scale of the $v'_{00}(r)$ function to be fixed at its equilibrium value and to only allow the amplitude to be adjusted so as to reproduce M_{00} . This still leaves one undetermined parameter that can be taken to be z_{22} . In an application of this approach to granular fluids, a similar indeterminacy was solved by insisting that the compressibility equation continues to hold in the nonequilibrium state. Here, this is not useful because $v_{22}(r)$ has little influence on h_{00} which would be the object fixed by such a relation. (In fact, this could be used as an alternate means of fixing z_{00} .) With no other exact or well-approximated property to fit, it seems appropriate to try to minimize the perturbation of the tail of the DCF. The tail of the full DCF is found to be

$$c_{22}(r) = K_{22} \frac{\exp(-z_{22}(r-1))}{r} \frac{r^2 z_{22}^2 - 3 z_{22}r - 3}{r^2 z_{22}^2}$$
$$-\frac{3}{r^3} \int_0^\infty c_{22}(x) x^2 dx \text{ for } r > \sigma, \qquad (47)$$

which is clearly short ranged if the last term on the right vanishes as it in fact does in the present approximation as a result of the condition given in Eq. (46). For large separations, the tail is therefore the same as that of the auxiliary function, a Yukawa term and this cannot be changed by any condition on z_{22} . At short range, the Yukawa term is modified and one possibility that suggests itself is to demand that at contact, the tail assume its equilibrium value, namely, zero. This implies that $\sigma z_{22} = \frac{3}{2} + \frac{1}{2}\sqrt{21} \approx 3.8$, which is the value used below.

IV. MOLECULAR DYNAMICS SIMULATIONS

In order to evaluate the model for the structure proposed above, I have performed molecular dynamics simulations of sheared hard spheres in three dimensions. The shearing state is imposed by means of Lees-Edwards boundary conditions consisting of periodic boundaries in all directions except that of the gradient (here, the y direction). If a particle exits the volume in the positive y direction (say, at y = L/2), it is

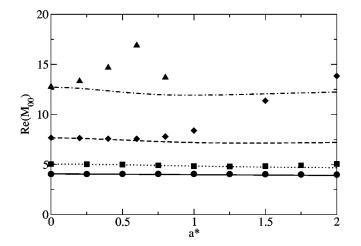


FIG. 1. $\text{Re}(M_{00})$ as a function of the reduced shear rate, a^* for densities of 0.1 (circles), 0.25 (squares), 0.5 (diamonds), and 0.75 (triangles). The lines are the predicted values calculated from Eq. (15). Note the nonmonotonic behavior at the highest density.

reentered at the opposite side of the volume (y = -L/2) with its velocity in the direction of flow shifted as $v_x \rightarrow v_x - aL$ and its position in the x direction shifted to x - aLt where t is the total time transpired in the simulation. Taken together, these constitute periodic boundaries in the local rest frame. The heating is controlled by periodically rescaling the velocities. Specifically, to maintain an average temperature T_0 , the velocities are rescaled to give an instantaneous temperature of $0.95T_0$ whenever the instantaneous temperature exceeds $1.05T_0$. The simulations reported here were performed using 500 atoms except where noted below. In all cases, a cubic simulation cell was used. The equilibration procedure consisted of first creating an equilibrium liquid at the desired density. After 10⁷ collisions, the shear rate was then instantaneously set to the desired value and the system allowed to relax under the Lees-Edwards boundary conditions for another 10⁷ collisions. Finally, the simulation was extended for another 10^7 collisions during which statistical averages were accumulated under the ergodic hypothesis. In order to estimate the accuracy of the quantities obtained, Erpenbeck's pooling method [35] was used whereby averages were accumulated over periods of 10⁵ collisions and stored. The reported values were subsequently computed by averaging these partial averages and the standard error of these partial averages, i.e., the standard deviation divided by the square root of the number of observations, used as an estimate of their accuracy. Except as noted below, the error bars in all figures are smaller than the symbols used to display the data. Finally, all simulations were performed for reduced densities of $n^* \equiv n\sigma^3 = 0.1, 0.25, 0.5, \text{ and } 0.75$. Based on the difference of the equilibrium PDF at contact from its low-density value, namely, $\chi_0 = 1$, these densities correspond to low density $(\chi_0 = 1.14)$, moderately dense $(\chi_0 = 1.4)$, dense $(\chi_0$ =2.15), and very dense (χ_0 =3) fluids, respectively. Shear rates are reported in units of the Boltzmann collision time $a^* = a/(4n^*\sqrt{\pi k_B T}).$

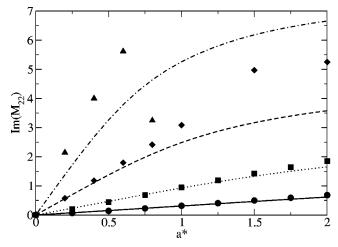


FIG. 2. Same as Fig. 1 but showing M_{22} .

A. The pair distribution at contact

Figures 1–3 show the projections M_{lm} of the PDF at contact onto the spherical harmonics for lm=00, 22, and 44 as a function of shear rate which accounts for angular dependencies of the form 1, $\hat{q}_x \hat{q}_y$, and $\hat{q}_x^2 - \hat{q}_y^2$, respectively. The spherical average of the PDF, g_{00} , shows little variation with shear rate for $n^*=0.1$ and 0.25 and only begins to show significant variation above $a^* = 0.5$ for $n^* = 0.5$ while at the highest density, significant variation is observed for all shear rates and, unlike at lower density, the curve is not monotonic. In all cases, the Enskog prediction is a slight decrease with increasing shear rate which is confirmed in the low-density data. The system at intermediate density is consistent with the model for small shear rates but shows an increase at higher shear rates as does the high-density system at all shear rates, in qualitative disagreement with the model. The major nonequilibrium contribution to the structure resides in the $Im(g_{22})$ components which show qualitatively similar behavior: agreement with the model at low density and all shear rates and for low shear rates at moderate density with significant disagreement at moderate density and high shear rates and at all shear rates at high density. The next largest

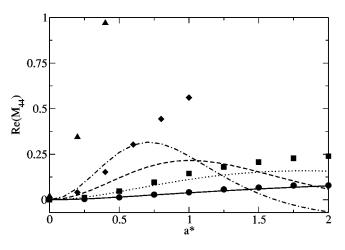


FIG. 3. Same as Fig. 1 but showing M_{44} .

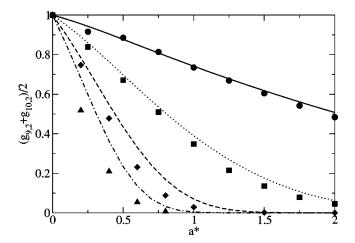


FIG. 4. The value of $\frac{1}{2}(g_{9,2}+g_{10,2})$ as defined in Eq. (48). The labeling is the same as in Fig. 1.

nonequilibrium contribution, $\text{Re}(g_{44})$, is seen to be nearly an order of magnitude smaller than $\text{Im}(g_{22})$ and it is also poorly described by the model.

These results show that the largest nonequilibrium contributions to the PDF occur in the four directions $(\pm 1/\sqrt{2}, \pm 1/\sqrt{2}, 0)$. To give a direct overview of the accuracy of the models, the average of the pdf at contact over a number of angular bins, defined as

$$g_{mn} = \int_{-1+m\delta_x}^{-1+(m+1)\delta_x} d\cos\theta \int_{n\delta_\phi}^{(n+1)\delta_\phi} d\phi g(\hat{\mathbf{q}}), \quad (48)$$

was monitored during the simulations for $\delta_x = \frac{1}{10}$ and $\delta_{\phi} = \pi/10$. Figure 4 shows a comparison between theory and simulation of $\frac{1}{2}(g_{9,2}+g_{10,2})$, e.g., of the pair distribution at contact averaged over the area -0.1 < x < 0.1 and $0.2\pi < \phi < 0.3\pi$, for the various densities. This patch is centered on the direction $(1/\sqrt{2}, 1/\sqrt{2}, 0)$ for which the deviations from equilibrium are largest. The most striking feature of these results is that the PDF drops with increasing shear until it

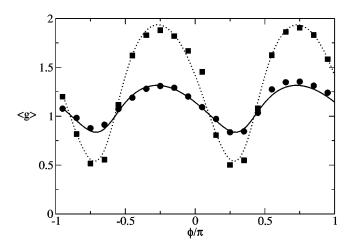


FIG. 5. The PDF at contact averaged over a solid angle defined by -0.1 < x < 0.1 and $m/10 < \phi/\pi < (m+1)/10$ for $-10 \le m \le 10$. The shear rate is fixed at $a^*=1.0$ and the information for $n^*=0.1, 0.25$ is labeled as in Fig. 1.

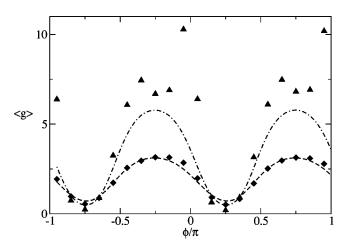


FIG. 6. The same as Fig. 5, but for $a^* = 0.6$ and $n^* = 0.5, 0.75$.

becomes vanishingly small, indicating that no collisions take place in that direction. The figure also shows the predicted values based on the generalized assumption of molecular chaos, Eq. (16), averaged (numerically) over the same solid angle. It is evident that the model works quite well at the lowest densities, is reasonable at the intermediate density, and is only qualitatively correct at the highest density. In order to visualize the full directional variation of the PDF at contact, Fig. 5 shows the spatial variation of the PDF averaged over the same sized solid angle for the whole range of values of ϕ from $-\pi$ to π for fixed shear rates of 1.0 for $n^*=0.1,0.25$ and Fig. 6 shows the same for $a^*=0.6$ and $n^* = 0.5, 0.75$. (The reason for choosing a lower shear for the higher densities will become apparent below.) For all but the highest densities, the spatial variation is consistent with the model, Eq. (15), whereas for $n^* = 0.75$ the agreement is poor. Indeed, the simulation data in the latter case are erratic and appear to be a superposition of a periodic function with spikes near $\phi = 0$ and $\phi = \pi$, which corresponds to the directions parallel and antiparallel to the flow (i.e., $\pm \hat{x}$). Figure 7 shows the same quantity for $n^* = 0.5$ and $a^* = 1.0$ and the same superposition of features is apparent. There are

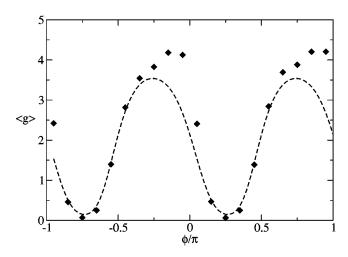


FIG. 7. The same as Fig. 5, but for $a^* = 1.0$ and $n^* = 0.5$.

three possible causes for deviations from the model: shearinduced ordering, inaccuracy of the one-body distribution, and breakdown of the assumption of molecular chaos. The structural anomalies at high shear rate and high density suggest the former.

It has been known for some time that hard spheres undergo an ordering transition at high shear rates [36]. The nature of the ordered phase remains uncertain and appears to depend on the type of thermostat used [27]. For the simple rescaling thermostat used here, an ordering first into planes perpendicular to the direction of the gradient (here, the y direction) and then into strings oriented along the direction of flow, and in a hexagonal pattern in the plane perpendicular to the flow, has been reported [36]. As a quantitative measure of such an ordering, the average density in a tube, oriented along the direction of flow has been monitored [2]. This is defined as

$$t(u) = \frac{1}{n\pi u^2 L} \left\langle \frac{1}{N} \sum_{i \neq j} \Theta(u^2 - q_{ij,y}^2 - q_{ij,z}^2) \right\rangle, \quad (49)$$

which can be written in terms of the PDF as

$$t(u) = \frac{1}{\pi u^2 L} \int d\mathbf{r} \ g(\mathbf{r}) \Theta(u^2 - y^2 - z^2)$$

= $\frac{L-2}{L} + \frac{2}{3L} u^4 + \frac{1}{\pi u^2 L} \int d\mathbf{r} \ h(\mathbf{r}) \Theta(r^2 - 1)$
 $\times \Theta(u^2 - y^2 - z^2)$ (50)

and gives the average density, relative to the bulk, observed along a tube of length L and radius u centered on an atom. In the limit of large L, the last term on the right will only give a nonzero contribution if long-range correlations in the direction of the flow are present (as they would be for a "string phase") so that any deviation from the equilibrium value could be attributed to the formation of such correlations. However, for the small systems considered here, the last term will give a nonzero contribution in all circumstances and variations of the tube density with the shear rate could be due to variations in the PDF which nevertheless do not involve long-ranged correlations. Figure 8, therefore, shows the tube density for a radius of half the hard-sphere diameter as a function of shear rate for systems of both 108 atoms and 500 atoms (giving L=6 and 10, respectively). For the lowest densities, the tube density actually decreases with increasing shear rate with the decrease being larger for the smaller system. Noting that the size of the effect is roughly in inverse proportion to the length of the systems and independent of the density, this would appear to be primarily a finite size effect leading to the conclusion that in neither case is there evidence of shear-induced changes in the density in the infinite system limit. For $n^* = 0.5$, the tube density is roughly constant until above $a^* = 0.6$ at which point it begins to rise steadily for both system sizes. Although the magnitude of the increase is also a function of system size, the relative variation between the two systems is much less than the overall

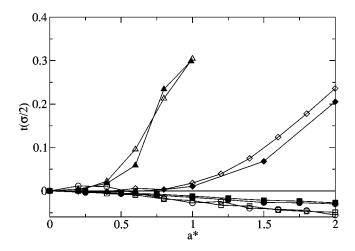


FIG. 8. The tube density $t(\sigma/2)$ as a function of the shear rate. The labeling is the same as in Fig. 1 except that here the lines are only a guide to the eye with the baseline, $t(\sigma/2)=0$ indicated by the thick line. Open symbols are from simulations of 108 atoms.

increase leading to the conclusion that the increase is due to the development of long-range order. This is consistent with our previously reported results indicating that shear-induced ordering takes place at this point [2]. Finally, at high density, the tube density increases dramatically above $a^*=0.2$, indicating an ordering transition at that point. This behavior, in this case nearly independent of system size, supports the conclusion that the deviation of the data from the molecular chaos hypothesis is due to shear-induced ordering for n^* =0.5 and $a^*>0.6$ and for virtually all of the data for the high-density system. It is also consistent with the structural data which show spikes in the PDF corresponding to an increase in collisions in the direction of the flow.

We are then only left with the poor agreement of the model for the g_{44} to explain. It seems likely that this is simply due to the inadequacy of the information supplied for the one-body distribution. Since the distribution is accurate only up to second moments of the velocity, it is reasonable that the calculation is only accurate up to second order in the unit vectors. Since these contributions are in any case small compared to the dominant g_{22} terms in the region of validity of the model, this aspect of the problem has not been pursued further.

B. The pair distribution function at finite separations

Here, attention is restricted to the domain of densities and shear rates below the ordering transition. In general, the components $g_{lm}(r)$ were estimated during the simulations by evaluating

$$g_{lm}(r) = \frac{1}{N_{samples}} \sum_{samples} \frac{1}{4\pi r^2 dr}$$
$$\times \sum_{i < j} \Theta(r_{ij} - r) \Theta(r + dr - r_{ij}) Y_{lm}^*(\hat{r}_{ij}), \quad (51)$$

where the inner sum is an estimate of $g_{lm}(r)$ based on a snapshot of the system and the outer sum indicates an aver-

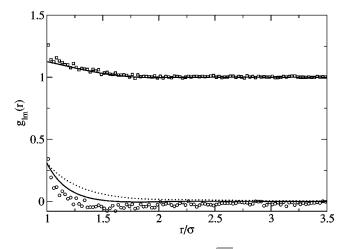
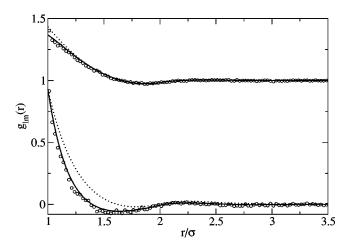
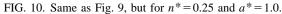


FIG. 9. The functions $\operatorname{Re}(g_{00}(r))/\sqrt{4\pi}$, upper curves, and $\operatorname{Im}(g_{22}(r))$, lower curves, for $n^*=0.1$ and $a^*=1.0$ from simulation(circles), the GMSA with the Yukawa closure (full lines), and the GMSA with the tail of the DCF set to zero (dotted lines).

age over many different snapshots. The results presented here are based on snapshots taken every 10 000 collisions. Ideally, one would like to replace the outer sum by a continuous time average in the spirit of the ergodic theorem but the computational expense would be prohibitive.

Figures 9–11 show $\operatorname{Re}(g_{00}(r))$ and $\operatorname{Im}(g_{22}(r))$ for n^* =0.1, 0.25, and 0.5 and a^* =1.0, 1.0, and 0.6, respectively, as determined from the simulations. While the spherically symmetric component is little changed from equilibrium, the main nonequilibrium component, $\operatorname{Im}(g_{22}(r))$, is comparable in magnitude near the core to the equilibrium PDF but decays rapidly and is difficult to measure beyond about two hard-sphere diameters. Also shown in these figures are the results of the GMSA model with both the Yukawa closure described above and the simpler closure in which the full DCF is set equal to zero outside the core. Both give a good description of the main features of the structure including the location of the sign changes and the amplitude and wavelength of the oscillations in g_{22} with the Yukawa closure being obviously superior in all cases. It is interesting that the





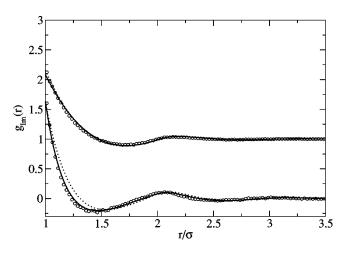


FIG. 11. Same as Fig. 9, but for $n^*=0.5$ and $a^*=0.6$.

largest discrepancy occurs for the lowest density. Based on the observed fluctuations in the identical determination of $g_{lm}(r)$ for this density in equilibrium, the statistical errors for this system appear to account for no more that half the deviation seen in Fig. 9. One noticeable characteristic of the simulation data for $n^*=0.1$ is that $\text{Im}(g_{22})$ appears to be systematically below the GMSA model and indeed systematically below zero away from the core. This suggests that the deviation might be a sign of the slow, algebraic decay predicted by mode-coupling theory [34] and which is not incorporated in the GMSA model.

Figures 12 and 13 show the same simulation data as Fig. 11, together with the numerical evaluation of the models of Hess [Eq. (20)] and Ronis [Eq. (27)] performed by means of a Monte Carlo integration using the VEGAS algorithm [37–39]. Because it can be formulated in real space, the Hess model requires one fewer integral than the Ronis model so that the evaluations are quicker and more accurate. In both

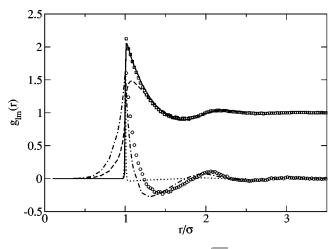


FIG. 12. The functions $\operatorname{Re}(g_{00}(r))/\sqrt{4\pi}$ and $\operatorname{Im}(g_{22}(r))$ for $n^*=0.5$ and $a^*=0.6$ from simulation (squares and circles, respectively), the Hess model with the smaller parameter (full and dotted lines, respectively), and with the larger parameter (dashed and dot-dashed lines, respectively).

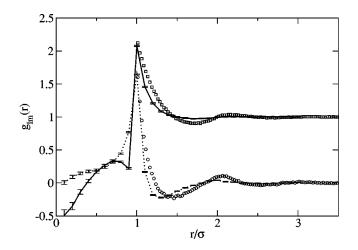


FIG. 13. The functions $\operatorname{Re}(g_{00}(r))/\sqrt{4\pi}$ and $\operatorname{Im}(g_{22}(r))$ for $n^*=0.5$ and $a^*=0.6$ from simulation (squares and circles, respectively), and the Ronis model (full and dotted lines, respectively). The error bars are the standard errors reported by the VEGAS algorithm used to evaluate the model.

cases, the parameters were adjusted so as to reproduce the calculated value of $Im(M_{22})$. Curiously, there are two values of the free parameter in the Hess model that satisfy this constraint. For the smaller of the two values, $\operatorname{Re}(g_{00}(r))$ is almost unchanged from equilibrium and $Im(g_{22}(r))$ is only nonzero in a very small region near the core. Both components are nonzero in a small region inside the core. The larger value of the parameter gives rise to a substantial deviation in $\operatorname{Re}(g_{00}(r))$, which is therefore not in good agreement with the simulation data. In contrast, $Im(g_{22}(r))$ is in qualitative agreement with the data outside the core. In this case, both components take on substantial values inside the core. The Ronis model, shown in Fig. 13, is similar to the large-parameter version of the Hess model. The spherically symmetric component is modeled somewhat better but $Im(g_{22}(r))$ is somewhat worse than with the Hess model. The behavior inside the core is also worse, with $\operatorname{Re}(g_{00}(r))$ even taking on negative values.

V. DISCUSSION

The goal of the work presented here has been to describe the density-density correlation function in a sheared hardsphere fluid over a range of densities, length scales, and shear rates. It was shown that the Enskog approximation for the velocity correlations provides a basis for calculating the the density-density correlation function at contact and that the results hold up well when compared to simulation, even for conditions of moderate density and high shear rates. Indeed, deviations from the Enskog predictions are primarily attributable to the high shear rate phase transition and, as noted previously [2], appear to signal its onset. For finite separations, the nonequilibrium GMSA was shown to provide a framework within which the known information about the correlation function at contact, coming from the Enskog approximation could be used to provide an accurate description of the dominant effects at finite separations. While

power-law decays arise naturally in the solution of the anisotropic OZ equation, the inverse-cubic decay in $g_{22}(r)$ is in contradiction to the $1/r^{17/3}$ decay predicted by recent modecoupling calculations [34]. Furthermore, those calculations indicate a $1/r^{11/3}$ decay in $g_{00}(r)$ for which there is no analog in the OZ solution. Of course, such algebraic decays could find their origin in the auxiliary functions and, indeed, might be used as boundary conditions in place of the Yukawa closure of the GMSA. However, the mode-coupling results are the result of a number of approximations (linearized Navier-Stokes-Langevin model solved perturbatively) and may not be giving the true asymptotic behavior. Altogether, the question of the actual form of these algebraic decays must be considered to be unresolved at this point since the data presented here are adequately fitted without them (except, possibly, for $n^* = 0.1$). More extensive simulations that can provide better statistics for the decay at separations significantly above two or three hard-sphere diameters would be required in order to resolve this issue. What can be said here is that even if algebraic tails exist, they must be significantly weaker than the dramatic nonequilibrium contributions seen near the core.

Two other, closely related, theories for the PDF were also considered and shown to capture some of the qualitative behavior of the PDF but both suffer from the unphysical prediction of nonzero probabilities inside the core. Before dismissing this class of theory on this basis, it is interesting to consider whether the main failing could be eliminated. In order to show that this is indeed the case, consider the second equation of the BBGKY hierarchy for hard spheres

$$\frac{\partial}{\partial t} + \sum_{i=1,2} \left(\mathbf{p}'_{i} \cdot \frac{\partial}{\partial \mathbf{q}_{i}} + \mathbf{q}_{i} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_{i}} + \frac{\partial}{\partial \mathbf{p}'_{i}} \cdot \mathbf{F}(x_{i}) \right)
+ \bar{T}_{-}(12) \left] \rho_{2}(x_{1}, x_{2}; t)
= -N \int d3 [\bar{T}_{-}(13) + \bar{T}_{-}(23)] \rho_{3}(x_{1}, x_{2}, x_{3}; t). \quad (52)$$

First, observe that in the most general case the distribution must have the form

$$\rho_2(x_1, x_2; t) = \Theta(r_{12} - \sigma) \bar{\rho}_2(x_1, x_2; t)$$
(53)

since the atoms cannot interpenetrate. Substituting this into Eq. (52), one finds two terms proportional to $\delta(r_{12}-\sigma)$: the first coming from the action of the spatial gradients on the step function in Eq. (53) and the second from the collisional operator $\overline{T}_{-}(12)$. These must cancel so that their coefficients must be equal and this just gives the relation between precollisional and postcollisional distribution functions used to derive Eq. (6). The remaining regular part of the kinetic equation then reads

$$\Theta(q_{12} - \sigma) \left[\frac{\partial}{\partial t} + \sum_{i=1,2} \left(\mathbf{p}'_i \cdot \frac{\partial}{\partial \mathbf{q}_i} + \mathbf{q}_i \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_i} + \frac{\partial}{\partial \mathbf{p}'_i} \cdot \mathbf{F}(x_i) \right) \right] \bar{\rho}_2(x_1, x_2; t)$$

$$= -N\Theta(q_{12} - \sigma) \int d3[\bar{T}_-(13) + \bar{T}_-(23)] \bar{\rho}_3(x_1, x_2, x_3; t), \qquad (54)$$

where an analogous decomposition of the three-body distribution has been introduced. Integrating over all momenta and discarding surface terms then yields

$$\Theta(q_{12} - \sigma) \left[\frac{\partial}{\partial t} + \mathbf{q}_{12} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_{12}} \right] y(\mathbf{q}_{12}; t)$$

$$= -\Theta(q_{12} - \sigma) n \int d\mathbf{p}_1 d\mathbf{p}_2 \int d3 [\bar{T}_-(13)$$

$$+ \bar{T}_-(23)] \bar{\rho}_3(x_1, x_2, x_3; t), \qquad (55)$$

where $y(\mathbf{q}_1, \mathbf{q}_2; t)$ is the nonequilibrium cavity function and is related to the PDF by $g(\mathbf{q}_1, \mathbf{q}_2; t) = \Theta(q_{12} - \sigma)y(\mathbf{q}_1, \mathbf{q}_2; t)$. This suggests that a more physical approximation would be to make a relaxation approximation [in the same spirit as the approximation leading from Eq. (19) to Eq. (20)] for the cavity function of the form

$$\Theta(q_{12} - \sigma) \left[\frac{\partial}{\partial t} y(\mathbf{q}_{12}; t) + \mathbf{q}_{12} \cdot \vec{a} \cdot \frac{\partial}{\partial \mathbf{q}_{12}} y(\mathbf{q}_{12}; t) - \int d\mathbf{r} A(\mathbf{q}_{12} - \mathbf{r}) [y(\mathbf{r}; t) - y_0(\mathbf{r})] \right] = 0.$$
(56)

There is no reason at this point to keep the step-function in this equation since any solution valid for all separations will be valid outside the core. Then, this gives in Fourier space

$$\frac{\partial}{\partial t} \tilde{y}(\mathbf{k};t) - \mathbf{k} \cdot \tilde{a}^{T} \cdot \frac{\partial}{\partial \mathbf{k}} \tilde{y}(\mathbf{k};t) = \tilde{A}(\mathbf{k}) [\tilde{y}(\mathbf{k};t) - \tilde{y}_{0}(\mathbf{k})]$$
(57)

and for steady-state shear flow the solution is

$$\widetilde{y}(\mathbf{k}) = \widetilde{y}_{0}(k) + \int_{0}^{\infty} dt \left(\frac{ak_{x}k_{y}(-at)}{k} \widetilde{y}_{0}'(k(-at)) \right)$$
$$\times \exp\left(-\int_{0}^{t} dt' \widetilde{A}(\mathbf{k}(-at')) \right).$$
(58)

An extension of the Hess model would be to take $\tilde{A}(\mathbf{k}) = \sum_{lm} A_{lm} Y_{lm}(\hat{k})$ for some set of constants A_{lm} adjusted to give the correct moments at contact. A similar extension of the Ronis model is also possible. An investigation of these models will be left to a future study.

In conclusion, it has been shown that the Enskog approximation for the pair correlations at contact, together with the GMSA model, provides a good description of the density autocorrelation function in a sheared fluid. The same techniques also give a good description of the PDF in granular fluids (modeled as inelastic hard spheres) [4] giving evidence that the approach is applicable to a variety of nonequilibrium systems. In both cases, simply knowing the value of the PDF at contact, from the Enskog approximation, and applying the standard formalism of liquid-state theory are enough to give a description of features of the system arising solely from the nonequilibrium state. Further work will include the extension of this model to the description of static correlation functions involving temperature and velocity.

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APPENDIX: SOLVING THE OZ MODEL FOR USF

The OZ equations written in terms of the auxiliary functions are

$$\widetilde{h}'_{lm}(k) = \widetilde{c}'_{lm}(k) + n \frac{1}{\sqrt{4\pi}} \sum_{|l'-l''| \le l \le l'+l''} \sum_{m'=-l'}^{l'} \times A(l,l',l'',m,m') \widetilde{c}'_{l'm'}(k) \widetilde{h}'_{l''m-m'}(k), \quad (A1)$$

and the boundary conditions, which follow directly from Eq. (38), are

$$\Theta(\sigma - r)h'_{lm}(r) = -\sqrt{4\pi}\delta_{l0}\delta_{m0} + (1 - \delta_{l0}) \times \sum_{n=0}^{(l/2)-1} B_{lm,n}r^{2n},$$
(A2)

$$\Theta(r-\sigma)c'_{lm}(r) = v'_{lm}(r),$$

where the constant coefficients are functionals of the structure function

$$\sum_{n=0}^{(l/2)-1} B_{lm,n} r^{2n}$$

= $-\frac{1}{r} \int_{\sigma}^{\infty} dr' \sum_{n=0}^{k-1} (4n+3) P_{2n+1} \left(\frac{r}{r'}\right) h_{lm}(r';t).$ (A3)

Note that Eq. (A3) is not a self-consistency condition: rather, it will automatically be satisfied for any solution of Eqs. (A1) and (A2) as can be verified using the relation

$$h_{lm}(r;t) = h'_{lm}(r;t) - \frac{1}{r^2} \sum_{n=0}^{(l/2)-1} (4n+3) \\ \times \int_0^r r' dr' P_{2n+1} \left(\frac{r'}{r}\right) h'_{lm}(r';t).$$
(A4)

Instead, the significance of the constants is revealed by considering the equivalent relation for the DCF,

$$c_{lm}(r;t) = c'_{lm}(r;t) - \frac{1}{r^2} \sum_{n=0}^{(l/2)-1} (4n+3) \\ \times \int_0^r r' dr' P_{2n+1}\left(\frac{r'}{r}\right) c'_{lm}(r';t), \quad (A5)$$

which implies that

$$(r-1)c_{lm}(r;t) = \Theta(r-1)v_{lm}''(r;t) - \Theta(r-1)\frac{1}{r^2}\sum_{n=0}^{(l/2)-1} (4n+3) \times \int_0^1 r' dr' P_{2n+1}\left(\frac{r'}{r}\right) [c_{lm}'(r';t) - v_{lm}'(r';t)], \quad (A6)$$

where

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$$v_{lm}''(r) = v_{lm}'(r) - \frac{1}{r^2} \sum_{n=0}^{(l/2)-1} (4n+3)$$
$$\times \int_0^r r' dr' P_{2n+1} \left(\frac{r'}{r}\right) v_{lm}'(r').$$
(A7)

The reason for defining $v'_{lm}(r)$ is precisely due to the nonuniqueness of this transformation, as discussed below Eq. (39) of the text. The point is that if we assumed a closure of the full DCF of the form $v_{lm}(r) = \phi_{lm}(r)$ $+ \sum_{n=1}^{[(l-1)/2]} A_{lm,n} r^{-(2n+1)}$, then only $\phi_{lm}(r)$ would contribute to $v'_{lm}(r)$ and we would find that $v''_{lm}(r) = \phi_{lm}(r)$. We would then complete the problem by adjusting the constants $B_{lm,n}$ so that the boundary condition is satisfied, meaning

$$\sum_{n=1}^{[(l-1)/2]} A_{lm,n} r^{-(2n+1)}$$

= $\frac{1}{r^2} \sum_{n=0}^{(l/2)-1} (4n+3) \int_0^r r' dr' P_{2n+1} \left(\frac{r'}{r}\right) v'_{lm}(r').$

However, in the present application, we are not concerned about the full DCF and so the $B_{lm,n}$ are simply treated as free parameters.

If we retain only the l=0,m=0 and $l=2,m=\pm 2$, components, the model can be reduced to the solution of a one dimensional OZ. The explicit form of the OZ equations in this case are

$$\begin{split} \tilde{h}_{00}^{\prime} &= \tilde{c}_{00}^{\prime} + n \sqrt{\frac{1}{4 \pi}} [\tilde{c}_{00}^{\prime} \tilde{h}_{00}^{\prime} + (\tilde{c}_{22}^{\prime} \tilde{h}_{2-2}^{\prime} + \tilde{c}_{2-2}^{\prime} \tilde{h}_{22}^{\prime})], \\ \tilde{h}_{22}^{\prime} &= \tilde{c}_{22}^{\prime} + n \sqrt{\frac{1}{4 \pi}} (\tilde{c}_{00}^{\prime} \tilde{h}_{22}^{\prime} + \tilde{c}_{22}^{\prime} \tilde{h}_{00}^{\prime}), \end{split}$$
(A8)

$$\tilde{h}'_{2-2} = \tilde{c}'_{2-2} + n \sqrt{\frac{1}{4\pi}} (\tilde{c}'_{00} \tilde{h}'_{2-2} + \tilde{c}'_{2-2} \tilde{h}'_{00}),$$

with the boundary conditions

$$\Theta(\sigma - r)h'_{00}(r) = -\sqrt{4\pi},$$

$$\Theta(\sigma - r)h'_{2\pm 2}(r) = -B_{2\pm 2,0},$$

$$\Theta(r - \sigma)c'_{00}(r) = v'^{(0)}_{00}(r),$$

$$\Theta(r - \sigma)c'_{2\pm 2}(r) = v'^{(0)}_{22}(r),$$

$$\lim_{\epsilon \to 0} h'_{00}(\sigma + \epsilon) = M_{00},$$

$$\lim_{\epsilon \to 0} h'_{2\pm 2}(\sigma + \epsilon) = M_{2\pm 2} + B_{2\pm 2,0}.$$

(A9)

First, note that $h_{l-m} = (-1)^m h_{lm}^*$, etc., which follows from the equivalent property of the spherical harmonics. Then, it is useful to separate the equations into their real and imaginary parts to get

$$\begin{split} \tilde{h}_{00}^{\prime} &= \tilde{c}_{00}^{\prime} + n \sqrt{\frac{1}{4\pi}} [\tilde{c}_{00}^{\prime} \tilde{h}_{00}^{\prime} + 2(\tilde{c}_{22,r}^{\prime} \tilde{h}_{22,r}^{\prime} + \tilde{c}_{22,i}^{\prime} \tilde{h}_{22,i}^{\prime})], \\ \tilde{h}_{22,r}^{\prime} &= \tilde{c}_{22,r}^{\prime} + n \sqrt{\frac{1}{4\pi}} (\tilde{c}_{00}^{\prime} \tilde{h}_{22,r}^{\prime} + \tilde{c}_{22,r}^{\prime} \tilde{h}_{00}^{\prime}), \quad (A10) \\ \tilde{h}_{22,i}^{\prime} &= \tilde{c}_{22,i}^{\prime} + n \sqrt{\frac{1}{4\pi}} (\tilde{c}_{00}^{\prime} \tilde{h}_{22,i}^{\prime} + \tilde{c}_{22,i}^{\prime} \tilde{h}_{00}^{\prime}), \end{split}$$

where $\tilde{h}'_{22,r} \equiv \operatorname{Re}(\tilde{h}'_{22})$, etc. Second, because of the linearity in the 22 components of the last two equations and the boundary conditions on the core values of the components of the structure function are constants, these equations are solved by taking

$$\vec{h}_{22,r}' = x \vec{h}'_{22,i},$$
(A11)
$$x = M_{22,r} / M_{22,i},$$

giving

$$\tilde{h}_{00}^{\prime} = \tilde{c}_{00}^{\prime} + n \sqrt{\frac{1}{4\pi}} [\tilde{c}_{00}^{\prime} \tilde{h}_{00}^{\prime} + 2(1+x^2) \tilde{c}_{22,i}^{\prime} \tilde{h}_{22,i}^{\prime}],$$
(A12)

$$\tilde{h}_{22,r}' = \tilde{c}_{22,r}' + n \sqrt{\frac{1}{4\pi}} (\tilde{c}_{00}' \tilde{h}_{22,r}' + \tilde{c}_{22,r}' \tilde{h}_{00}'),$$

provided $\operatorname{Re}(v_{22}^0) = x \operatorname{Im}(v_{22}^0)$, which we are free to impose. Now, define $h(r;u) = h'_{00}(r) + uh'_{22,i}(r)$, which satisfies

$$\begin{split} \tilde{h}(k,u) &= \tilde{c}(k,u) + n \sqrt{\frac{1}{4\pi}} [\tilde{c}_{00}' \tilde{h}_{00}' + u(\tilde{c}_{00}' \tilde{h}_{22,r}' + \tilde{c}_{22,r}' \tilde{h}_{00}') \\ &+ 2(1+x^2) \tilde{c}_{22,i}' \tilde{h}_{22,i}'] \\ &= \tilde{c}(k,u) + n \sqrt{\frac{1}{4\pi}} \tilde{c}(k,u) \tilde{h}(k,u), \end{split}$$
(A13)

where the last line follows if and only if $u = \pm \sqrt{2(1+x^2)}$. The boundary conditions are then

$$\Theta(\sigma - r)h(r;u) = -\sqrt{4\pi} - u \operatorname{Im}(B_{22,1}), \quad (A14)$$

$$\Theta(r - \sigma)c(r,u) = v_{00}^{\prime(0)}(r) + u v_{22}^{\prime(0)}(r).$$

Finally, introduce scaled quantities defined by $h(r;u) = [\sqrt{4\pi \pm |u|} \operatorname{Im}(B_{22,1})] H_{\pm}(r)$ and $c(r;u) = [\sqrt{4\pi} + |u| \operatorname{Im}(B_{22,1})] C_{\pm}(r)$,

which give

$$\tilde{H}_{\pm}(k) = \tilde{C}_{\pm}(k) + n_{\pm}\tilde{C}_{\pm}(k)\tilde{H}_{\pm}(k),$$

$$\Theta(\sigma - r)H_{\pm}(r) = -1,$$
(A15)

$$\Theta(r-\sigma)C_{\pm}(r) = \left[\sqrt{4\pi} \pm |u| \operatorname{Im}(B_{22,1})\right]^{-1} v_{00}^{\prime(0)}(r)$$

$$\pm |u| \left[\sqrt{4\pi} \pm |u| \operatorname{Im}(B_{22,1})\right]^{-1} v_{22}^{\prime(0)}(r),$$

which can be recognized as the OZ equation for a (possibly negative) density $n_{\pm} = n[1 \pm |u| \sqrt{(1/4\pi)} \text{Im}(B_{22,1})]$ and some particular closure condition (so that this resembles the usual GMSA). For the simplest case, in which one takes $v_{00}^{\prime(0)}(r) = 0$, we have $H_{\pm}(r) = h_{py}(r;n_{\pm})$ and the solution is trivial. If the tail functions, $v_{00}^{\prime(0)}(r)$ and $v_{22}^{\prime(0)}(r)$ are Yukawa

terms, then we can make use of the solution of Hoye and Blum for a closure consisting of a sum of Yukawa terms [33]. For completeness, we collect together the various transformations to see that

$$h_{00}'(r) = \frac{\sqrt{4\pi}}{2n} [n_{+}H_{+}(r) + n_{-}H_{-}(r)],$$

$$h_{22,i}'(r) = \frac{\sqrt{4\pi}}{2|a|n} [n_{+}H_{+}(r) - n_{-}H_{-}(r)], \quad (A16)$$

$$h_{22,r}'(r) = xh_{22,i}'(r).$$

The value of $Im(B_{22,1})$ is, of course, fixed by requiring that

$$\lim_{\epsilon \to 0^+} h'_{22,i}(\sigma + \epsilon) = -\operatorname{Im}(B_{22,1}) + \operatorname{Im}(M_{22}), \quad (A17)$$

while the full PDF is

$$h(\mathbf{r}) = h'_{00}(r)Y_{00}(r) + 2h''_{22,r}(r)\operatorname{Re}Y_{22}(\hat{r})$$

$$- 2h''_{22,i}(r)\operatorname{Im}Y_{22}(\hat{r})$$

$$= \frac{1}{\sqrt{4\pi}}h''_{00}(r) + \sqrt{\frac{5}{8\pi}}h''_{22,r}(r)(\hat{r}_{x}^{2} - \hat{r}_{y}^{2})$$

$$- \sqrt{\frac{5}{2\pi}}h''_{22,i}(r)\hat{r}_{x}\hat{r}_{y}, \qquad (A18)$$

where

$$h_{22}''(r) = \int_0^\infty r'^2 dr' U_2(r',r) h_{22}'(r';t)$$

= $\Theta(r-1) \bigg[h_{22}'(r';t) + \frac{\operatorname{Im}(B_{22,1})}{r^3} - \frac{3}{r^3} \int_1^r r'^2 dr' h_{22}'(r';t) \bigg].$ (A19)

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